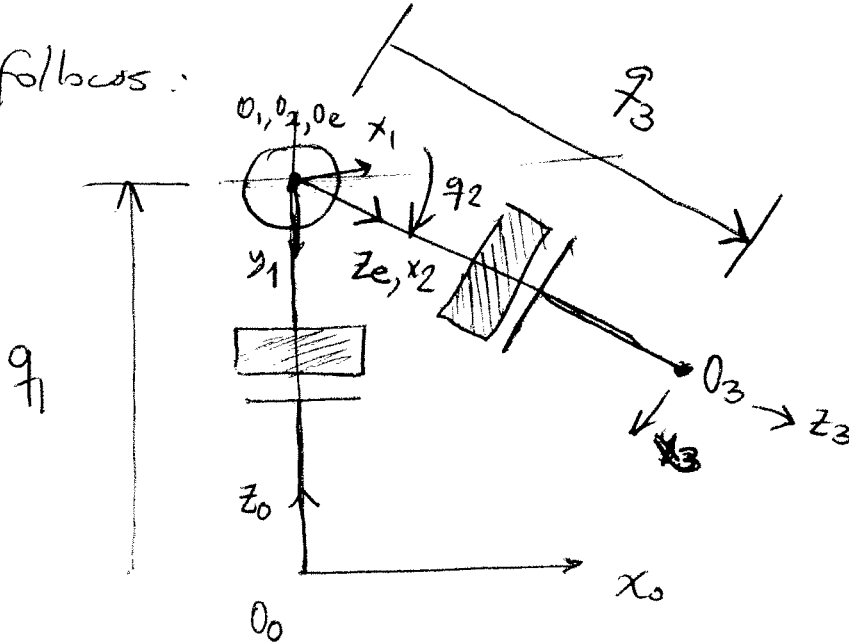


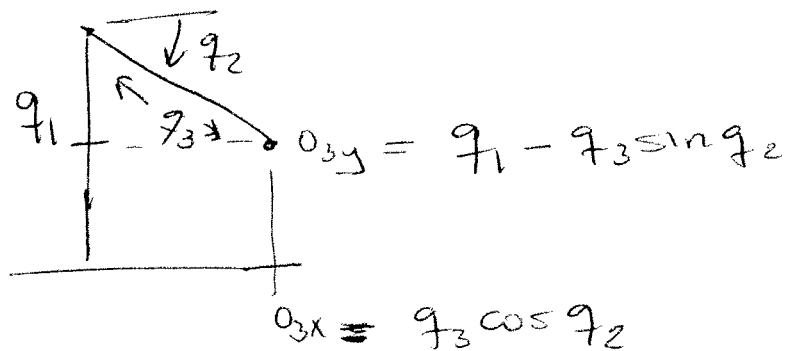
MCE/EEC 647/747 Midterm solution - Spring '15
 - Dr. Richter -

1. From the DH table, the robot and frames are as follows:



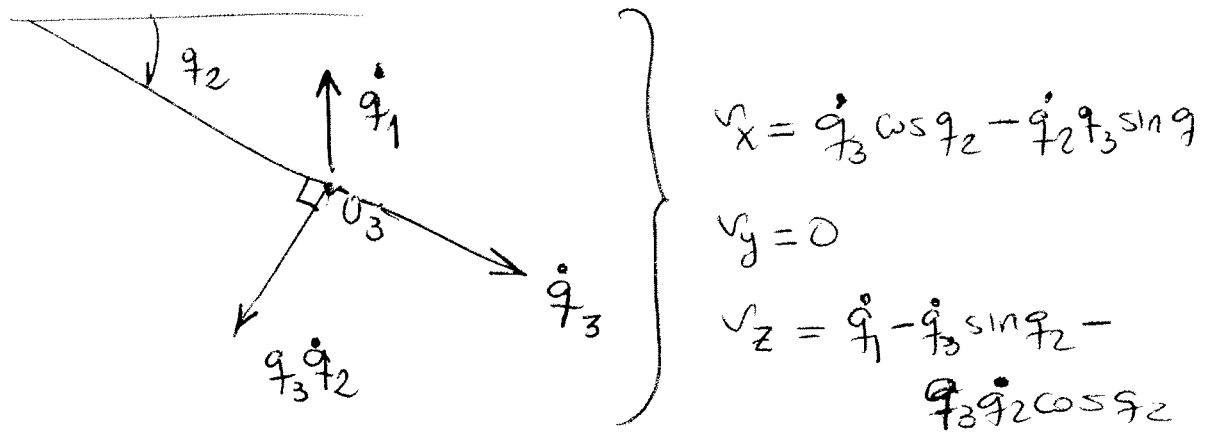
Clearly this is a planar robot (incapable of moving into the y_0 direction)

Position of O_3 :



$${}^0 O_3 = \begin{bmatrix} q_3 \cos q_2 \\ 0 \\ q_1 - q_3 \sin q_2 \end{bmatrix}$$

We can find the world velocity of O_3 by vector addition of velocities:



$$\left. \begin{aligned} v_x &= \dot{q}_3 \cos q_2 - \dot{q}_2 l_3 \sin q_2 \\ v_y &= 0 \\ v_z &= \dot{q}_1 - \dot{q}_3 \sin q_2 - \dot{q}_2 l_3 \cos q_2 \end{aligned} \right\}$$

In vector-matrix form:

$$\dot{O}_3 = \begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & -l_3 s_2 & c_2 \\ 0 & 0 & 0 \\ 1 & -l_3 c_2 & -s_2 \end{bmatrix}}_{\text{Jacobian, (singular)}} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \end{bmatrix}$$

Jacobian, (singular).

The robot can't produce a nonzero velocity in the y direction y is restricted to 0.

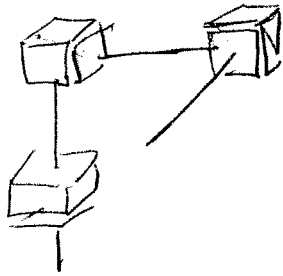
Manipulability ellipsoid: $\eta(q) = \sqrt{\det(J^T J)}$

$$J^T J = \begin{bmatrix} 0 & 0 & 1 \\ -l_3 s_2 & 0 & -l_3 c_2 \\ c_2 & 0 & -s_2 \end{bmatrix} \begin{bmatrix} 0 & -l_3 s_2 & c_2 \\ 0 & 0 & 0 \\ 1 & -l_3 c_2 & -s_2 \end{bmatrix} = \begin{bmatrix} 1 & -l_3 c_2 & -s_2 \\ -l_3 c_2 & l_3^2 & 0 \\ -s_2 & 0 & 1 \end{bmatrix}$$

Because J is square, no need to find $\det(J^T J)$

$$\text{we know } \eta(q) = |\det(J)| = 0$$

2. If the three P joints are orthogonal



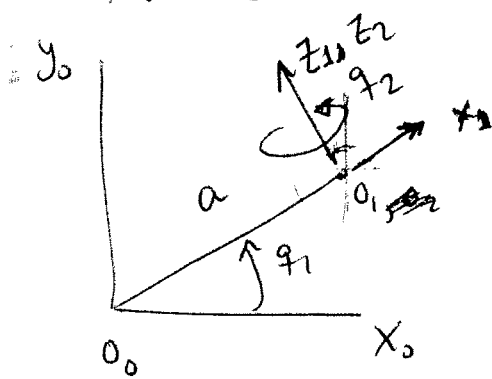
then $v = \begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix} = \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \end{bmatrix} = \mathbf{I} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \end{bmatrix}$

↑
Jacobian

Then there cannot be singularities.

If at least 2 joints are parallel, the manipulator is always singular (in 3D).

3. From the D-H table, the robot and frames are as follows:



From this figure:

$$z_1^0 = z_2^0 = \begin{bmatrix} -a \sin q_1 \\ a \cos q_1 \\ 0 \end{bmatrix}$$

$$z_0^0 = \hat{k}$$

$$o_1^0 = \begin{bmatrix} a \cos q_1 \\ a \sin q_1 \\ 0 \end{bmatrix}$$

To compute the linear velocity Jacobian, we need only

$$Jv_1 = z_0^0 \times (o_2^0) - \text{point of interest}$$

$$Jv_2 = z_1^0 \times (o_2^0 - o_1^0)$$

So only o_2^0 is needed!

$$o_2^0 = A_2^0 o_2^2 = A_2^0 \begin{bmatrix} 0 \\ 1 \\ 0 \\ 1 \end{bmatrix}$$

$$A_1^0 = \text{Rot}_{z, \varphi_1} \cdot \text{Rot}_{x, -\pi/2} \cdot \text{Trans}_{x, a}$$

$$A_1^0 = \left[\begin{array}{ccc|c} \cos \varphi_1 & 0 & -\sin \varphi_1 & a \cos \varphi_1 \\ \sin \varphi_1 & 0 & \cos \varphi_1 & a \sin \varphi_1 \\ 0 & -1 & 0 & 0 \\ \hline 0 & 0 & 0 & 1 \end{array} \right] \quad O_1^0$$

find this from the rotations only (one 3x3 multiplication)

$$A_2^1 = \text{Rot}_{z, \varphi_2}$$

Multiply: $A_1^0 A_2^1 = A_2^0 =$

$$\left[\begin{array}{c|c} \begin{array}{c} \times \\ \times \\ \times \end{array} & \begin{array}{c} O_1^0 \\ \text{still!} \end{array} \\ \hline \begin{array}{c} \circ \end{array} & 1 \end{array} \right] \quad \left. \begin{array}{l} \text{only these} \\ \text{are needed!} \end{array} \right\} \begin{array}{l} \text{because} \\ A_2^1 \text{ is} \\ \text{a pure} \\ \text{rotation} \end{array}$$

$$O_2^0 = A_2^0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} a \cos \varphi_2 - \cos \varphi_1 \sin \varphi_2 \\ a \sin \varphi_2 - \sin \varphi_1 \sin \varphi_2 \\ -\cos \varphi_2 \end{bmatrix}$$

Jacobian computation:

$$J_{v_1} = z_0 \times O_2^0 = \hat{K} \times O_2^0 = \begin{vmatrix} \hat{z} & \hat{j} & \hat{k} \\ 0 & 0 & 1 \\ O_{2x}^0 & O_{2y}^0 & O_{2z}^0 \end{vmatrix}$$

$$J_{r_1} = \begin{bmatrix} s_1 s_2 - a s_1 \\ a c_1 - c_1 s_2 \\ 0 \end{bmatrix}$$

$$J_{r_2} = Z_2 \times (0_2^0 - 0_1^0) = \begin{bmatrix} -s_1 \\ c_1 \\ 0 \end{bmatrix} \times \begin{bmatrix} a s_2 - c_1 s_2 - a c_1 \\ a s_1 - s_1 s_2 - a s_1 \\ -c_2 \end{bmatrix}$$

some computation required...

$$J_{r_2} = \begin{bmatrix} -c_1 c_2 \\ -c_2 s_1 \\ s_2 \end{bmatrix}$$

$$\text{so } J_r = \begin{bmatrix} -s_1(a - s_2) & -c_1 c_2 \\ c_1(a - s_2) & -c_2 s_1 \\ 0 & s_2 \end{bmatrix}$$

For $\theta_1 = 0$, $\theta_2 = -\pi/2$:

$$J_r = \begin{bmatrix} 0 & 0 \\ a+1 & 0 \\ 0 & -1 \end{bmatrix}$$

There is no singularity because J_r is full-rank

$$\text{Manipulability: } J_r^T J_r = \begin{bmatrix} (a+1)^2 & 0 \\ 0 & 1 \end{bmatrix}$$

$$\sqrt{\det(J_r^T J_r)} = a+1$$

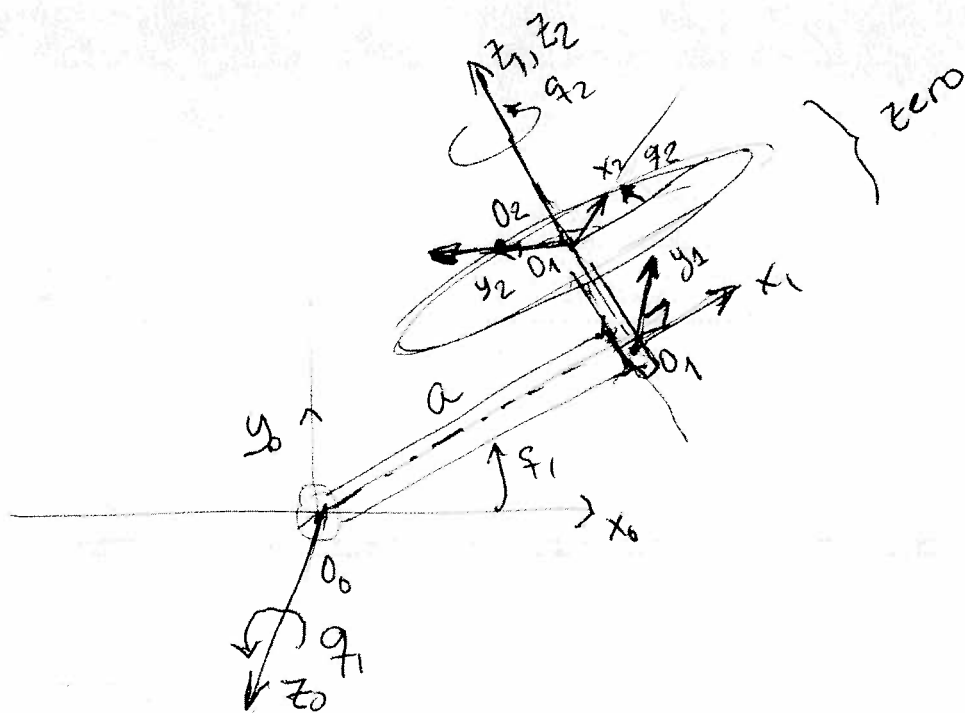
b. Angular velocity Jacobian:

$$J_{w_1} = z_0^0 = \hat{n}_0; \quad J_{w_2} = z_1^0 = \begin{bmatrix} -s_1 \\ c_1 \\ 0 \end{bmatrix}$$

$$J_w = \begin{bmatrix} 0 & -s_1 q_1 \\ 0 & +c_1 q_1 \\ 1 & 0 \end{bmatrix}$$

the 2 columns are always linearly independent
($\sin q_1$ and $\cos q_1$ can't be zero at the same time)

3b. Extended discussion (beyond the exam)



General singularities: If $s_2 = a \rightarrow$ singularity.
 (|a| ≤ 1 needed)
 Suppose $s_2 \neq a$:

$$J_V = \begin{bmatrix} -s_1(a-s_2) & -c_1 c_2 \\ c_1(a-s_2) & -c_2 s_1 \\ 0 & s_2 \end{bmatrix}$$

For the Jacobian to have rank less than 2

We need $s_2 = 0 \rightarrow c_2 = \pm 1$

so $J_V = \begin{bmatrix} -s_1 a & \pm c_1 \\ c_1 a & \pm s_1 \\ 0 & 0 \end{bmatrix}$

For the 2 columns to be dependent, we would

also need $\begin{cases} -s_1 a = \pm c_1 \gamma \\ c_1 a = \pm s_1 \gamma \end{cases}$ for some scalar γ

- If $a = 0$ this is impossible, because c_1 and s_1 cannot be both zero.

- If $a \neq 0$: If $\gamma = 0$, singularity is impossible (same reason)

If $\gamma \neq 0$: $\gamma = \pm \frac{s_1 a}{c_1}$
 $\gamma = \pm \frac{c_1 a}{s_1} \rightarrow \frac{s_1^2}{c_1^2} = \pm 1$

of which only $\frac{s_1^2}{c_1^2} = 1$ is possible, so we would need $s_1^2 = c_1^2$

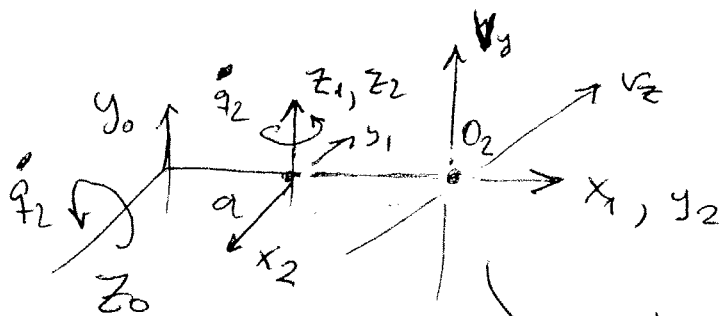
But the combination of signs for s_1 and c_1 in the columns of J_V (for $s_2=0$) make this impossible.

→ There are no linear velocity singularities, $\text{rank}(J_V) = 2$ for any q_1, q_2 , unless $|a| < 1, \sin q_2 = a$

This means that the dimension of the velocity space for any configuration is always 2. (for 0_2)

Sometimes the velocity has all 3 (x, y, z) components different than zero, sometimes not.

For example, for $q_1 = 0, q_2 = -\pi/2$



at this configuration, the absolute velocity of O_2 has nonzero v_y & v_z components, but zero v_x component.

This is confirmed by finding the general

$$\eta(q) = \sqrt{\det(J_v^T J_v)}$$

$$J_v^T J_v = \begin{bmatrix} (a - s_2)^2 & 0 \\ 0 & 1 \end{bmatrix}$$

$$\eta(q) = |a - s_2|$$

$\eta(q) = 0$ only if $|a| \leq 1$ and $\sin(q_2) = a$

4. The closed-loop transfer function is

$$T(s) = \frac{\frac{1}{s^2}(K_D s + K_P)}{1 + \frac{K_D s + K_P}{s^2}}$$

$$T(s) = \frac{K_D(s + K_P/K_D)}{s^2 + K_D(s + K_P/K_D)}$$

If K_P/K_D is very small (~ 0)

$$T(s) = \frac{K_D s}{s^2 + K_D s} = \frac{K_D}{s + K_D}$$

$T(0) = 1$, so there will be no offset (sse) for a step input reference.

The percent overshoot will be zero, because $T(s)$ is first-order

The time constant is $1/K_D$, so the

settling time will be $\frac{4}{K_D}$.